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Application of: Yuki NAKAMURA, et al.

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For : PHASE CHANGE OPTICAL RECORDING MEDIUM

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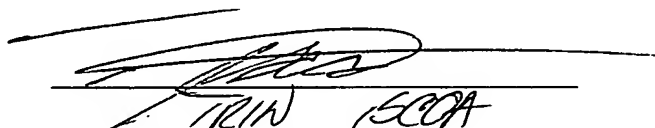
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I hereby certify that the above-identified application (consisting of a 64-page specification (including 11 pages of claims (48 claims) and a 1 page Abstract), and 8 sheets of formal drawings (Figs. 1-11)), 3 copies of an Application Transmittal Form, unexecuted Declaration and Power of Attorney, certified copies of Japanese Application Nos. 2001-002258, 2001-005734 and 2001-057392, and authorization to charge deposit account for the filing fee of \$1,496.00, are being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, D.C. 20231.


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Application
for
United States Letters Patent

To all whom it may concern:

Be it known that,

Yuki NAKAMURA and Masaki KATOH

have invented certain new and useful improvements in

PHASE CHANGE OPTICAL RECORDING MEDIUM

of which the following is a full, clear and exact description:

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TITLE

PHASE CHANGE OPTICAL RECORDING MEDIUM

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BACKGROUND

Field

This patent specification relates in general to an optical recording medium, and more particularly to a phase-change recording medium and methods for optimally initializing and recording feasible for carrying out read/write/erase operations at high and multiple recording velocities.

Discussion of Background

Optical information recording media have recently come into wide use as viable information data storage and archival device of large capacity.

A phase-change recording medium is capable of repeated read/write/erase operations by means of laser beam irradiation utilizing phase transition between amorphous and crystalline states. For this type of the media in particular, overwrite operations can be carried out using a single light beam and a relatively simple optical system for readout, which is advantageous over magneto-optical memories that may involve difficulties in overwriting. The optical recording capability of the phase-change recording medium can therefore be utilized, for example, in rewritable compact discs (CD-RWs) and rewritable digital versatile discs (DVD-RWs).

Phase-change materials for forming such recording media have attracted much attention recently to implement the aforementioned media

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capabilities. For example, U.S. Patent No. 3530441 discusses chalcogenide alloys such as Ge-Te, Ge-Te-Sn, Ge-Te-S, Ge-Se-S, Ge-Se-Sb, Ge-As-Se, In-Te, Se-Te and SeAs.

To improve stability and crystallization speed are Ge-Te alloy materials, proposals have been made to add Au (Japanese Laid-Open Patent Application No. 61-219692), Sn and Au (Japanese Laid-Open Patent Application No. 61-270190), or Pd (Japanese Laid-Open Patent Application No. 62-19490). Further proposals to improve write/readout characteristics for repeated operations involve use of Ge-Te-Se-Sb and Ge-Te-Sb alloys with specified compositions (Japanese Laid-Open Patent Applications No. 62-73438 and 63-228433).

These alloy materials, however, have not been fully satisfactory in achieving various desirable characteristics of the rewritable phase-change optical recording medium.

In particular, there remain several problems of great importance yet to be solved to achieve desirable characteristics. This may be achieved by attaining sufficient sensitivity during either writing or erasing operation, preventing decrease in erasure ratio caused by leftover portions during overwriting steps, and improving durability of the media properties of written or non-written portions in the recording medium.

Another recording medium is proposed in Japanese Laid-Open Patent Application No. 63-251290, including a single recording layer with a crystallized state of practically more than ternary composition.

"Practically more than ternary" means therein that the alloy system includes at least 90 atomic % of a ternary compound (e.g., In_3SbTe_2) in the recording layer. It is also stated in the document that write/erasure characteristics are improved with this alloy composition. However, the

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composition still has shortcomings such as erasure ratio of relatively small magnitude and laser power to be reduced for write/erase operations.

In addition, still another recording medium is proposed in Japanese Laid-Open Patent Application No. 1-277338, including $(Sb_a Te_{1-a})_{1-y} M_y$ with $0.4 \leq a \leq 0.7$ and $y \leq 0.2$, in which M includes at least one additive selected from the group consisting of Ag, Al, As, Au, Bi, Cu, Ga, Ge, In, Pb, Pt, Se, Si, Sn and Zn.

This alloy system essentially consists of Sb_2Te_3 , and several medium characteristics with this system are said to have been improved such as, high speed write/erase cycle operations by including excess amount of Sb, and high speed erasure by the addition of M elements. In addition, it is also stated that the erasing ratio is relatively large for light beams in the continuous (or DC) mode. However, no description is found in that document with respect to the erasing ratio for overwrite operations.

In this context, it may be noted that erasure leftover portions have been found by the present inventors during erasing experiment on the alloy system, and its recording sensitivity is considered not satisfactory.

In a similar manner, further recording media are proposed including respective recording layers such as in Japanese Laid-Open Patent Application No. 60-177446 including $(In_{1-x} Sb_x)_{1-y} M_y$ with $0.55 \leq x \leq 0.80$ and $0 \leq y \leq 0.20$, where M includes at least one element selected from the group consisting of Au, Ag, Cu, Pd, Pt, Al, Si, Ge, Ga, Sn, Te, Se and Bi; the other in Japanese Laid-Open Patent Application No. 63-228433 including an alloy $GeTe-Sb_2Te_3-Sb$ (in excess). However, the recording media composed of these alloy systems have not attained sufficient media characteristics such as recording sensitivity and erasing ratio.

Further, there are proposals for optical recording media provided with respective recording layers including alloy systems such as, a Ge-Te-Sb alloy with added N, as in Japanese Laid-Open Patent Application No. 4-163839; a Te-Ge-Se alloy formed such that at least one of constituent
5 elements thereof is incorporated as a nitride, as in Japanese Laid-Open Patent Application No. 4-52188; and a Te-Ge-Se alloy adsorbed with N, as in Japanese Laid-Open Patent Application No. 4-52189. The optical recording media composed of these alloy systems, however, have not acquired satisfactory characteristics for the recording media.

10 In spite of numerous proposals for alloy materials for forming recording layers of the optical recording media, as described hereinabove, there persist a need to solve several problems of great importance and to thereby acquire desirable media characteristics such as sufficient sensitivity during writing or erasing operation by preventing decrease in
15 erasure ratio caused by leftover portions during overwrite steps, also improving durability of the structure and property of recorded and non-recorded portions in the recording medium.

Compact discs (CDs) have come into wide use recently as viable information storage media. Along with the rapid growth of the CDs,
20 another type of compact discs, which are writable only once discs (or CD-R's) have been developed and recently placed into the market. However, since information data once recorded on the CD-R disc cannot be corrected because of its write-once feature mentioned just above, the CD-R disc has a shortcoming, in that the disc may become useless if even one non-
25 correctable error is inputted during the writing steps. Another type of the storage medium has therefore been sought, that is capable of obviating the above disadvantage of the CD-R disc.

One example of such storage media is a rewritable compact disc utilizing magneto-optical materials. The magneto-optical disc, however, has drawbacks such as difficulty in overwriting and incompatibility with CD-ROM and CD-R discs. A phase-change type recording medium has
5 been made practical recently having disc characteristics compatible with the above media, among others.

Research and development results achieved so far are exemplified by the rewritable phase-change recording media and compact discs incorporating the recording media by Furuya, et al., Proceedings of the 4th
10 Symposium on phase change optical recording (1992) 70; Kanno, et al., Proceedings of the 4th Symposium on phase change optical recording (1992) 76; Kawanishi, et al., Proceedings of the 4th Symposium on phase change optical recording (1992) 82; Handa, et al., Japanese Journal of Applied Physics, Vol. 32 (1993) 5226; Yoneda, et al., Proceedings of the
15 5th Symposium on phase change optical recording (1993) 9; and Tominaga, et al., Proceedings of the 5th Symposium on phase change optical recording (1993) 5.

These rewritable phase-change recording media, however, have not satisfied overall characteristics, such as compatibility with CD-ROMs and
20 CD-Rs, write/erase capability, recording sensitivity, repeatability of rewriting and readout operations, and durability during storage. The above noted shortcomings in media characteristics are believed primarily due to relatively low erasure ratios caused by the composition and/or structure of the recording materials previously employed for forming the
25 phase-change recording media.

Accordingly, it is desirable to develop novel recording materials capable of attaining higher erasure ratios and being suitable for more

sensitive write/erase operations, to thereby be able to implement phase-change compact discs having improved rewritable capabilities.

In an effort to find such improved material systems and thereby solve the above noted shortcomings, the present inventors have previously proposed several AgInSbTe recording materials. These materials are discussed in Japanese Laid-Open Patent Applications No. 3-240590, 4-78031, 4-123551, 4-232779, 5-345478 and 8-22644.

These mixed alloy systems have excellent sensitivity during writing or erasing operation, and particularly with large erasure ratios, thereby being advantageous for forming recording layers utilizing the mark-edge recording method.

However, since the AgInSbTe mixed alloy systems have been developed to this date for use in recording media primarily with linear recording speed of up to 10 m/sec, the recording media incorporating these alloy system have drawbacks such as insufficient recording cycle capability for the practical use as the recording media with higher recording speed.

Since the recording layer is in the amorphous state immediately after the layer formation, the layer has to be subjected to so called initialization process, in which it is crystallized by laser annealing process steps to thereby become crystallized having a high enough reflectivity suitable for data recording. This process of the initialization has a considerable effect on the resulting recording characteristics such as overwrite capability, in particular, of optical recording media incorporating such recording layer.

Several improvements have been proposed for the initialization process of recording media including phase-change recording materials.

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For example, Japanese Laid-Open Patent Application No. 8-77614 discusses an apparatus with a tandem type optical system to implement a uniform, high speed initialization of the phase change optical recording medium. Also discussed in that document are specified shapes of laser beams to be irradiated onto the recording medium for the initialization.

However, since no description is found on intensities or irradiation energy of the laser beams, recording media with satisfactory recorded signal quality are not considered feasible by that disclosure alone. Also not found therein is a description of the multiple speed recording and recording characteristics at linear velocity of 4.8 m/sec or more.

Japanese Laid-Open Patent Application No. 9-73666 discusses an optical information recording medium, and a method and an apparatus for forming the medium, in which optically readable marks are provided outside data recording regions on the medium for media ID information be stored for the optical recording medium.

Another optical information recording medium, and a method and an apparatus for initializing the medium, are discussed in Japanese Laid-Open Patent Application No. 9-212918, and involves melting at least a portion of the recording layer during the initialization. The laser beams used during the initialization steps are shaped such that the longer axis (i.e., major axis) of an ellipsoidal or rectangular beam is aligned perpendicular to a recording track, to thereby improve the characteristics of recorded signals. In addition, a layer construction of the recording medium is specified.

Although the above document refers to improvement in recording characteristics achieved by melting at least a portion of the recording layer during initialization, no description is found on irradiation energy of the laser beams. As earlier noted, the irradiation energy is believed to have a

considerable effect on the melting process.

As a result, the improvement in recording characteristics referred to in the document may not be entirely satisfactory. In addition, no description was found of multi-speed recording and recording characteristics at linear velocity of 4.8 m/sec or more.

Japanese Laid-Open Patent Application No. 10-241211 discusses improved initialized characteristics are achieved by carrying out a layer processing step prior to the initialization during recording media fabrication. However, the initialization is carried out twice, resulting in decreased productivity. In addition, again no description is found of multi-speed recording and recording characteristics at linear velocity of 4.8 m/sec or more.

An optical information recording medium, and the method and apparatus for initializing the medium, are discussed in Japanese Laid-Open Patent Application No. 10-289447, in which the beam shape axis of a laser irradiating the medium is not parallel to recording tracks, to thus defocus the beam. According to this document one effected is to decrease unevenness in reflectivity resulting from the initialization, also in initialization effects which may be caused by overlap of repeated exposures to beam irradiation, and thereby keep the beam on track. However, no description is found of irradiation energy of the laser beams, and again no description is found of multiple speed recording and recording characteristics at linear velocity of 4.8 m/sec or more.

Since of a recent tendency to keep increasing the speed of media recording, it is highly desirable for information recording media to be devised that would have satisfactory recording capabilities at various velocities (i.e., multi-speed recording) exemplified by, for example, CAV

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(constant angular velocity) recording and excellent signals characteristics after recording.

For information data recording into the thus initialized optical recording medium, the determination of optimum recording power with
5 sufficient accuracy is important for practical usage.

Japanese Patent Publication 63-29336 discusses a method for recording information signals on an optical recording medium by a write/readout apparatus, including the steps of scanning energetic beam spots such as those from a laser source over the recording medium while
10 irradiating, and modulating the intensity of the spots corresponding to the information signals, to thereby achieve information recording.

Also discussed in the publication is a method for determining optimum recording conditions regarding power, pulse width and so forth, of the recording laser beams, by reading out the signals recorded on the
15 medium, and by subsequently monitoring the width of readout signals and the length of recorded marks.

However, it is believed to be difficult in practice to always determine optimum conditions by this method even after utilizing information signals actually recorded on the recording medium by
20 conventional write/readout apparatuses.

The publication discusses a method which utilizes the width of readout signals as the representative value and monitors the width (i.e., the difference in signal level between the signals from non-recorded media portions and from recorded portions), to seek the conditions optimum for
25 respective write/readout apparatuses.

However, the width of readout signals changes not only with recording power, but also with other parameters such as the numerical

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aperture of the optical system, rim intensity (i.e., spatial intensity distribution of laser beams upon incidence onto a collimator lens), the size and shape of beam spots, and dirty optics and change with time, and other factors.

5 For example, dirty optics can cause optical efficiency to vary by as much as 20 % to 40 % between optical systems in respective write/readout apparatuses. Therefore, the value determined as the optimum recording power as discussed above may be significantly affected by these parameters.

10 It has been difficult in practice to determine the optimum recording power with an enough accuracy (e.g., approximately $\pm 5\%$). As a result, difficulties have been encountered in recording media production to account for deviations in the effect of media recording found among write/readout apparatuses for the same laser power. This necessitates
15 additional minute adjustments of recording power for each apparatus, that causes drawbacks such as, for example, decrease in the productivity of recording media.

 In addition, the determination in advance of the optimum power has not been sufficiently effective, because of possible damage caused by
20 excessive laser power during test writing.

 That is, the rewritable medium should normally have certain advantages due to its characteristics as writable media so that after determining an appropriate laser power level from test recording made on recording tracks, data recording can be carried out with the thus
25 determined power onto the same recording racks for erase/write or overwrite step, which is in contrast to write once media for which extra tracks exclusively for test writing are needed to determine the power level

in advance.

In practice, however, the above advantages have not been fully realized, since damage to recording tracks are caused by the excessive level of laser power during test recording. As a result, extra tracks
5 exclusively for test writing have had to be provided in practice even for writable recording media, thereby resulting in undue waste of recording tracks, or recording area.

The present inventors have previously proposed an improved method for determining optimum recording power, in which the power is suitably
10 determined either without being affected by both amplitude of recorded signals, m , and recording power, W , or without being affected by the amplitude alone.

In addition, the optimum recording power can be determined with relative ease in this method with a sufficient accuracy particularly for
15 practical use in write/readout apparatuses devised for mass production. Further, addition of the above mentioned extra tracks is avoided and the accuracy of determined optimum laser power has been increased.

It has been realized by the present inventors, however, that further improvements may be made to achieve more efficient information
20 recording, particularly for recording power as high as 15 to 18 mW.

SUMMARY

Accordingly, it is an object of the present disclosure to provide an optical information recording medium and a method for initializing and
25 recording the recording medium, having most, if not all, of the advantages and features of similar employed optical recording media and methods, while eliminating many of the aforementioned disadvantages.

The following brief description is a synopsis of only selected features and attributes of the present disclosure. A more complete description thereof is found below in the section entitled "Description of Preferred Embodiments".

5 The phase-change optical recording medium disclosed herein includes at least a recording layer containing at least materials capable of carrying out read/write/erase operations through phase changes of the materials, and the recording layer preferably essentially consists of Ag, In, Sb and Te, with the proportion in atomic percent of a(Ag): b(In): c(Sb):
10 d(Te), with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$ and $5 \leq d \leq 26$, provided that $a + b + c + d \geq 97$.

 Alternatively, the recording layer may essentially consist of Ag, In, Sb, Te and Ge, with the proportion in atomic percent of a(Ag): b(In): c(Sb): d(Te): e(Ge), with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$, $5 \leq d \leq 26$
15 and $0.3 \leq e \leq 3$, provided that $a + b + c + d + e \geq 97$. In addition, the layer preferably has a composition satisfying the relation, $88 \leq c + d \leq 98$.

 According to another aspect, the optical recording medium is formed incorporating a substrate, and contiguous layers deposited on the substrate in order as follows, a first dielectric layer, a recording layer, a second
20 dielectric layer, a metal/alloy layer, and an ultraviolet light curing resinous layer, in which the recording layer essentially consists of phase change recording materials having one of the compositions described above. These first dielectric layer, recording layer, second dielectric layer and metal/alloy layer are each formed preferably having a thickness ranging
25 from 30 nm to 220 nm, 10 nm to 25 nm, 10 nm to 50 nm, and 70 nm to 250 nm, respectively.

In addition, the recording medium is rewritable at least once at a linear recording velocity ranging from 9 m/sec to 30 m/sec. Furthermore, the metal layer preferably essentially consist of Al and at least one kind of additive with a content ranging from 0.3 weight percent to 2.35 weight percent, which is selected from the group consisting of Ta, Ti, Cr and Si. Also, the metal/alloy layer preferably essentially consist of Ag and at least one kind of additive with a content ranging from 0 to 4 weight percent, which is selected from the group consisting of Au, Pt, Pd, Ru, Ti and Cu.

According to another aspect, a sputtering target for forming a recording layer is disclosed, in which the recording layer is incorporated into an optical recording medium capable of carrying out read/write/erase operations through phase changes of materials therein.

The sputtering target preferably essentially consists of Ag, In, Sb and Te, with the proportion in atomic percent of a(Ag): b(In): c(Sb): d(Te), with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$ and $5 \leq d \leq 26$, provided that $a + b + c + d \geq 97$.

Alternatively, the sputtering target may essentially consist of Ag, In, Sb, Te and Ge, with the proportion in atomic percent of a(Ag): b(In): c(Sb): d(Te): e(Ge), with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$, $5 \leq d \leq 26$ and $0.3 \leq e \leq 3$, provided that $a + b + c + d + e \geq 97$. In addition, the sputtering target preferably has a composition satisfying the relation, $88 \leq c + d \leq 98$.

According to another aspect, a method is disclosed for initializing a phase-change optical recording medium by irradiating the recording medium with a scanning beam spot emitted from a high power semiconductor laser device. The recording medium is capable of carrying out optically read/write/erase operations of information data.

The energy density input by the beam spot during one period of through scan is equal to, or less than, 1000 J/m^2 , or alternatively, equal to, or larger than, 600 J/m^2 . In addition, the scanning speed of the beam spot is in the range of 3.5 m/sec to 6.5 m/sec , and the intensity of the
5 emission from the semiconductor laser device is equal to, or greater than, 330 mW .

Furthermore, the width of an overlapped portion, which is formed as an overlap of irradiated portions, between two neighboring irradiation tracks on the recording medium during two consecutive rotations in
10 initializing steps, is equal to, or less than, $0.5 W_r$, where W_r is the width at half maximum of the spatial laser power distribution in the direction perpendicular to a scanning direction.

According to another aspect, an apparatus is disclosed that is configured to perform at least an initialization operation onto a phase-
15 change optical recording medium by irradiating the recording medium with a scanning beam spot emitted from a high power semiconductor laser device, in which the initialization operation includes at least the steps described above.

According to another aspect, a method is disclosed for carrying out
20 read/write/erase operations of information data on a rewritable phase-change optical recording medium through the phase change induced in a recording layer included in the recording medium by laser beam irradiation, in which the recording layer preferably essentially consists of Ag, In, Sb and Te elements.

25 The present method for selecting an optimum recording power includes at least the steps of (1) writing information data, as test recording runs, with recording power of a laser beam consecutively varied in the

range of 15 mW to 18 mW to thereby generate a recorded pattern including low and high reflective portions, (2) reading out signals from the low and high reflective portions on the recording medium to obtain a recorded signal amplitude, m , corresponding to the recording power, P , (3)
5 calculating a normalized gradient, $g(P)$, using the equation, $g(P) = (m/\Delta m)/(P/\Delta P)$, where ΔP is an infinitesimal change in the vicinity of P , and Δm is an infinitesimal change in the vicinity of m , (4) determining an optimum recording power, after assessing adequacy of the magnitude of the recording power based on the thus calculated normalized gradient, $g(P)$, (5)
10 selecting a specific number, S , from the numbers in the range of 0.2 to 2.0 based on the calculated normalized gradient, $g(P)$, (6) obtaining the value of recording power, P_s , which matches with the specific number, S , presently selected, (7) selecting a specific number, R , based on the thus obtained recording power, P_s , from the numbers in the range of 1.0 to 1.7, and (8) multiplying the recording power, P_s , by the specific number, R ,
15 whereby an optimum recording power, P_0 , is obtained.

In addition, these specific numbers, S and R , may be recorded in advance in the optical recording medium, to thereby be utilized to select an optimum recording power under actual media running conditions. For
20 the recording medium, the numbers, S and R , are in the range of $1.2 \leq S \leq 1.4$, and $1.1 \leq R \leq 1.3$, respectively, and the recording medium herein disclosed is recordable at a recording velocity ranging from 4.8 m/sec to 14.0 m/sec.

The present disclosure and features and advantages thereof will be
25 more readily apparent from the following detailed description and appended claims when taken with drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a section view illustrating the optical recording medium according to one embodiment disclosed herein;

FIG. 2 is a schematic diagram illustrating an initialization apparatus
5 according to one embodiment disclosed herein;

FIG. 3 is a schematic diagram illustrating an initialization apparatus according to another embodiment disclosed herein;

FIG. 4 contains a graph illustrating the first 3T land jitter results as a function of initialization power P and scanning speed of initialization
10 head V;

FIG. 5 contains a graph illustrating energy density as a function of initialization power P and scanning speed of initialization head V;

FIG. 6 contains a graph illustrating 3T land jitters after 1000 cycles as a function of initialization power P and scanning speed of initialization
15 head V;

FIG. 7 contains a graph illustrating reflectivity fluctuation ΔR_{gh} as a function of initialization power P and scanning speed of initialization head V;

FIG. 8 contains a graph illustrating the range of suitable P, V values
20 for achieving optimal initialization results;

FIG. 9 illustrates the pulse shape of input light beams of 5T width applied to the phase-change recording medium according to one embodiment disclosed herein;

FIG. 10 illustrates the pulse shape of input light beams applied to
25 the phase-change recording medium of Example 1; and

FIG. 11 is a block diagram illustrating the major parts of the write/readout system according to one embodiment disclosed herein.

DESCRIPTION OF PREFERRED EMBODIMENTS

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In the detailed description which follows, specific embodiments on information recording media and materials for forming such recording media are described together with the methods for initializing and recording the recording media. It is understood, however, the present disclosure is not limited to these embodiments, and it is appreciated that the materials and methods for optical recording media disclosed herein may also be adaptable to any form of information recording. Other embodiments will be apparent to those skilled in the art upon reading the following description.

The recording medium disclosed herein is characterized by quaternary phase-change recording materials including compositional elements such as Ag, In, Sb and Te, as the major components. The recording materials have several characteristics suitable for use in optical recording media, such as excellent sensitivity to, and speed of, recording (i.e., amorphous phase formation) and erasure (crystalline phase formation), and also having desirable erasure ratios.

The phase-change recording materials preferably have the composition specified in general by the relation among the proportion of the above noted compositional elements, Ag, In, Sb and Te, with the proportion in atomic percent of $a(\text{Ag}): b(\text{In}): c(\text{Sb}): d(\text{Te})$, with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$ and $5 \leq d \leq 26$, provided that $a + b + c + d \geq 97$.

Alternatively, the recording materials may preferably have the composition specified by the relation of $a(\text{Ag}): b(\text{In}): c(\text{Sb}): d(\text{Te}): e(\text{Ge})$, with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$, $5 \leq d \leq 26$ and $0.3 \leq e \leq 3$, provided that $a + b + c + d + e \geq 97$. In addition, particularly in the

present disclosure, a further relation may preferably supplemented as $88 < a + b + c + d < 98$.

The results on the composition of the recording layers disclosed herein have been obtained from emission spectral analysis. Other
5 methods may also be used for the analysis, such as X-ray microanalysis, Rutherford backscattering, Auger analysis, fluorescent X-ray spectroscopy and other similar methods. The results obtained from the latter methods may be used to compare with those from the emission spectral analysis. For the emission spectral analysis, the known error of measurement is, in
10 general, within 5%.

The structure of the materials in the recording layer may be examined by a diffraction method using either X-rays or electron beams. The crystalline state, for example, can be distinguished from the amorphous state using an electron beam diffraction method. This is, the
15 presence of diffraction spots and/or Debye rings in diffraction patterns is generally taken to be indicative of the crystalline state, while halo rings are indicative of the amorphous state. In addition, the diameter of the crystallites may be calculated from the peak width at half maximum of the X-ray diffraction patterns according to Scherrer's equation.

20 The nature of chemical bonds of oxides and nitrides included in the recording layer may be analyzed by spectroscopic methods such as, for example, FT-IR and XPS.

Recording layers are formed by sputtering methods using sputtering targets disclosed herein, preferably having a thickness ranging from 10 to
25 50 nm, more preferably from 12 to 25 nm. Layer thickness of less than 10 nm causes considerable decrease in absorbency and may become incapable of functioning as a proper recording layer, while difficulties in

achieving uniform phase transition result for the thickness greater than 50 nm at high speed recording.

It is known that a recording layer suitable for optical data recording can be formed using a sputtering target in which two components are included, one SeTe alloy and the other AgInTe_2 alloy having a composition of at least in the vicinity of the stoichiometric composition of either chalcopyrite or zincblende. The thus formed recording layer is subsequently subjected to appropriate layer processing such as, for example, initialization steps, whereby a recording layer is completed with desirable recording characteristics such as large erasure ratios and repeated write/erase capabilities.

The crystallite size of the above mentioned AgInTe_2 alloy, which has a structure of at least in the vicinity of either chalcopyrite or zincblende structure, can be determined by the X-ray diffraction method. That is, from the peak width at half maximum obtained for the main peak in X-ray diffraction (at diffraction angle of 24.1° for $\text{CuK}\alpha$ X-rays having $\lambda = 1.54\text{\AA}$), the crystallites size can be calculated. It is desirable to calibrate using a well defined standard set of the crystallite size in advance to ascertain the accuracy of the determination.

For the AgInTe_2 alloy with the crystallite size exceeding 45 nm, stable record/erase operations becomes difficult even after proper initialization process on the recording layer.

In addition, by using Ar sputtering gaseous compositions which include an adjusted amount of N gas of at most 10 mol%, desirable properties of the recording layer can be obtained depending on the N composition, so as to attain appropriate disc characteristics such as linear velocity of rotation and disc layer structure.

The use of the above noted mixed Ar/N gaseous compositions can also yield improved durability in record/erasure operations. The Ar/N gaseous compositions may be prepared either by mixing gaseous constituents in a predetermined mixing ratio prior to the introduction into a sputtering chamber, or by adjusting the proportion of respective incoming gaseous constituents such that a predetermined molar ratio be attained inside the sputtering chamber following the introduction.

The amount of N in the recording layer is preferably at most 5 atomic % to achieve appropriate disc characteristics. In addition to the above noted overwrite characteristics in repeated operations, concrete examples of improved disc characteristics are found on percentage modulation and storage life for the recorded marks (or amorphous marks), among others.

Although the details are yet to be clarified, the mechanism for these effects is considered as follows: The incorporation of N into the recording layer tends to increase the coarseness of the film structure caused by the decrease in layer density and the increase in minute defects. This causes the structural order of the layer to be more relaxed than that prior to the N incorporation, which, in turn, tends to suppress the transition from the amorphous state to the crystalline state. As a result, the stability of amorphous marks increases, thereby improving the storage life for the recorded marks. Furthermore, the linear velocity of the transition is controlled by adding appropriate amount of N into the recording layer.

The N elements are preferably incorporated into the recording layer chemically bonded to at least one of Ag, In, Sb and Te elements. When the chemical bond is formed with Te, in particular, such as exemplified by Te-N and Sb-Te-N, pronounced effects can be achieved with the

improvement in the number of repeated overwrite cycles.

Such chemical bonds may be analyzed by spectroscopic methods such as, for example, FT-IR and XPS. In FT-IR spectra, for example, the Te-N bond exhibits an absorption peak in the 500-600 cm^{-1} spectral range, while the Sb-Te-N bond has an absorption peak in the 600-650 cm^{-1} range.

In addition, it is effective for the recording layer to incorporate other elements or impurities to further improve media characteristics. For example, these additives are preferably selected from the group consisting of B, N, C, P and Si, as discussed in Japanese Laid-Open Patent Application No. 4-1488, and another group consisting of O, S, Se, Al, Ti, V, Mn, Fe, Co, Ni, Cu, Zn, Ga, Ge, Sn, Pd, Pt and Au. The addition of Ge elements are particularly effective in improving the durability of recorded marks and the number of overwrite cycles.

The thus formed recording layer is subsequently incorporated into an optical recording medium which will be described herein below in reference to FIG. 1.

A phase-change optical recording medium disclosed herein preferably includes a supporting substrate 1, and the following layers formed contiguously on the supporting substrate in order as follows: a first dielectric (heat resisting, protective) layer 2, a recording layer 3, a second dielectric (heat resisting, protective) layer 4, a reflective (heat dissipating) layer 5, and an overcoat (upper protective) layer 6. Further, a printed layer 7 and a hard coat layer 8 may additionally be formed on the overcoat layer 6 and the mirror face of the substrate, respectively.

Although both first and second dielectric layers 2,4 need not be formed placing the recording layer 3 therebetween as shown in FIG. 1, the formation of the former layer 2 is preferred in case of the substrate 1

formed of relatively low melting point materials such as polycarbonate, for example.

The supporting substrate 1 is formed of materials preferably sufficiently transparent to light in the wavelength range for use in
5 recording and readout operations of the recording medium.

Suitable materials for forming the substrate 1 include glass, ceramics and resinous materials. Of these materials, resins are preferably employed for their satisfactory transparency and moldability.

Specific examples of the resins include polycarbonate resins, acrylic
10 resins, epoxy resins, polystyrene resins, acrylonitrile-styrene copolymeric resins, polyethylene resins, polypropylene resins, silicone resins, fluororesins, acrylonitrile-butadiene-styrene (ABS) resins and urethane resins. Among these resins, polycarbonate resins and acrylic resins are preferably used for their excellent moldability, optical properties and
15 relatively low cost.

While the substrate 1 is usually disc-shaped, it may also be card-shaped or sheet-shaped.

In addition, the substrate may be provided with grooves, in general, and the grooves are formed preferably under the following conditions for
20 use in rewritable compact disc (CD-Rewritable). The grooves formed to help guide the laser beams during the read/write operations preferably have a width ranging from 0.35 μm to 0.70 μm , more preferably from 0.45 μm to 0.65 μm ; a depth thereof ranging from 15 nm to 60 nm, more preferably from 20 nm to 50 nm.

25 By implementing these substrate conditions together with the recording material and medium construction described earlier, a rewritable compact disc can be formed with excellent compatibility.

To be more specific, the magnitude of push-pull signals after recording, PPM, is an important characteristic for the compact disc (CD Standard), in which PPM values are required to be in the range between 0.04 and 0.15, preferably between 0.06 and 0.14, and most preferably
5 between 0.08 and 0.12.

It has been difficult for phase change rewritable compact discs to satisfy these PPM conditions and all other major requirements for read/write characteristics simultaneously at the linear recording speed of 10 m/sec or greater. However, this becomes feasible with the advent of
10 the phase change recording media disclosed herein, fulfilling the overall characteristics required for practical rewritable compact discs.

The dielectric (heat resisting, protective) layers are formed primarily consisting of dielectric materials for their suitable thermal and optical properties.

15 Examples of suitable dielectric materials for forming the dielectric layers include metal oxides such as SiO, SiO₂, ZnO, SnO₂, Al₂O₃, TiO₂, In₂O₃, MgO and ZrO₂; nitrides such as Si₃N₄, AlN, TiN, BN and ZrN; sulfides such as ZnS, In₂S₃ and TaS₄; carbides such as SiC, TaC, B₄C, WC, TiC and ZrC; diamond-like carbon, and mixtures thereof.

20 These materials may be used individually or in combination. In addition, they may further include impurities, where relevant. The dielectric layers may be formed to have a multilayered structure. Their melting temperatures are preferably higher than that of the recording layer.

The first and second dielectric layers 2,4 can be formed by, for
25 example, vacuum evaporation, sputtering, plasma CVD, light assisted CVD, ion plating, or electron beam evaporation, or other similar methods. Of these, the sputtering method is preferably utilized for its excellent

productivity and properties of those layers formed.

The materials and thickness for forming respective dielectric layers may be determined independent of one another after considering optical and thermal properties.

5 The first dielectric layer 2 preferably has a thickness ranging from 20 nm to 200 nm, more preferably from 30 nm to 120 nm. When the thickness thereof is less than 20 nm, the layer may not serve as a satisfactory heat resisting protective layer, while thickness of more than 200 nm causes several difficulties such as peeling-off at interlayer portions with relative ease and reduced recording sensitivity.

10 The thickness of the second dielectric layer 4 preferably ranges from 15 nm to 40 nm, more preferably from 20 nm to 35 nm. When the thickness thereof is less than 15 nm, the layer may not serve as a satisfactory heat resisting protective layer and can decrease recording sensitivity. In contrast, thickness of more than 45 nm can cause difficulties such as peeling-off at interlayer portions with relative ease and reducing the recording sensitivity in repeated recording operations, especially when recording at a linear velocity as low as from 1.5 to 5.6 m/sec.

15 In addition, the dielectric layers 2,4 may be formed to have a multilayered structure, as indicated earlier.

20 The recording layer 3 is formed on top of the thus formed first dielectric layer 2. The quaternary phase-change recording materials including compositional elements such as Ag, In, Sb and Te together with its composition suitable for forming the data recording as detailed earlier.

25 Alternatively, the recording layer 3 may be formed of phase change materials other than the AgInSbTe material. Examples of such alternative

phase change materials include alloys such as GeTe, GeTeSe, GeTeS, GeSeSb, GeAsSe, InTe, SeTe, SeAs, Ge-Te-(Sn, Au, Pd), GeTeSeSb, GeTeSb, and AgInSbTe.

5 The composition of these compounds may properly be adjusted to attain optimum recording sensitivity depending on the linear recording velocity or velocity range that is desired.

10 Furthermore, additional elements or impurities may be incorporated into the compounds to further improve media characteristics. The additional elements are preferably selected from the same group of elements as mentioned earlier for the AgInSbTe compounds together with Ga and Zr, additionally included. The above impurities are selected from those which are not already included as major components in respective recording materials.

15 The recording layer may be formed by, for example, vacuum evaporation, sputtering, ion plating, CVD, or other similar methods. Of these, the sputtering method is preferably utilized for its excellent productivity and low costs.

Subsequently, the reflective (heat dissipating) layer 5 is formed on top of the second dielectric (heat resisting, protective) layer 4.

20 Suitable materials for forming the reflective layer 5 include metals such as Al, Au, Ag and Cu and alloys thereof. Of these materials, Al alloys and Ag metal and its alloys are preferably employed for their excellent durability and low costs. These metals and alloys may each include added impurities, of which Ta, Ti, Cr and Si elements are effective
25 for the Al alloys, while Au, Pt, Pd, Ru, Ti and Cu are suitable for the Ag alloys.

The reflective layer 5 can be formed by, for example, vacuum evaporation, sputtering, plasma CVD, light assisted CVD, ion plating, electron beam evaporation, or other similar methods. In order for the reflective layer 5 to properly serve as a heat dissipating layer, the thickness thereof is preferably ranging from 50 nm to 200 nm, more preferably from 70 nm to 180 nm.

Thickness thereof greater than that above noted can cause an excessive heat dissipation that decreases recording sensitivity, while decrease in the overwrite cycle characteristics is found except recording sensitivity retained for smaller layer thickness.

As suitable properties for the reflective layer material, therefore, high heat conductivity and also high melting point are preferable.

Furthermore, an overcoat (upper protective) layer 6 is preferably formed on top of the reflective layer 5 to serve as an oxidation resistant layer. This layer is generally formed with ultraviolet curing resinous materials which may be added by spin coating or dipping methods.

The thickness thereof preferably ranges from 7 μm to 15 μm . Layer thickness of less than 7 μm may result in an increase of C1 errors (or block error rate) after affixing an overlying printed layer, while thickness of more than 15 μm can increase the internal stress which influences mechanical properties of the recording disc.

In addition, the overcoat layer 6 preferably has a sufficient hardness to prevent scratches caused by, for example, wiping the layer surface with a cloth. Further, electrically conductive composition may be incorporated into the overcoat layer, where relevant, to render it antistatic and thus prevent dirt from sticking onto the layer surface.

On the overcoat layer 6, at least one of printed layers 7 may be formed, when relevant, to thereby serve as a label. In contrast, a hard coat layer may additionally be formed on the mirror face of the substrate, to thereby increase surface strength against scratches. Examples of
5 material for use in the printed layer 7 may be selected from the group of conventional photo-curing inks which are printed generally by the screen printing method.

The materials and the method for forming the hard coat layer may be selected from ones similar to those for the protective layer 6. In addition,
10 two recording discs of appropriate overall thickness may be adhered with two overcoat layers back to back so as to form a single recording disc.

As electromagnetic radiation and energetic beams useful for initializing, recording, reading-out, or erasing the recording medium disclosed herein, laser light, ultraviolet light, visible light, infrared light or
15 microwave radiation may be utilized. Of these radiation and beams, light beams from a semiconductor laser device are preferably used because the laser's small size and compactness makes it suitable for incorporation into a drive unit for operating the recording media.

Since the recording layer is in the amorphous state immediately after
20 the layer formation, as described earlier, the layer has to be subjected to the so called initialization process, in which the layer is crystallized by laser annealing process steps to thereby become crystallized to a high enough reflectivity suitable for data recording. The process of the initialization has a considerable effect on the resultant recording
25 characteristics such as overwrite capability, in particular, of optical recording media incorporating such recording layer.

There will be described herein below the apparatus and process for carrying out the initialization process according to embodiments disclosed herein.

FIG. 2 is a schematic diagram illustrating an initialization apparatus according to one embodiment.

Referring to FIG. 2, the initialization apparatus includes at least a semiconductor laser device 11 as a light source, a collimator lens 12 for collimating laser beams, a beam splitter 13 for dividing reflected beams, an objective lens 14, another collimator lens 15, and an auto-focusing (AF) unit 16 including at least a detector and an actuator.

The laser source can be a semiconductor laser, a gas laser, and other similar laser devices. Of these devices, a high power semiconductor laser device is preferred for its small size and low costs.

The output power thereof is in general in the range between 400 to 1000 mW. Among the beam shapes thereof suitable for use in initialization, ellipsoidal or rectangular shape in near field pattern may preferably be utilized, with the lengths of the major and minor axes ranging from 10 to 500 μm and from 0.5 to 10 μm , respectively.

When the laser beams are aligned such that the longer axis thereof is at least close to perpendicular to recording tracks, there is an increase in the disc area (or medium area) covered by the laser beams per disc rotation. As a result, initialization efficiency can be increased, thereby helping reduce initialization time with this alignment of the laser beams.

The output beam of the semiconductor laser device 11 as the light source is collimated through the collimator lens 12, and then focused at least in the vicinity of the recording layer included in the medium by the objective lens 14 to irradiated the recording layer with radiation energy,

whereby data recording is achieved.

Portions of the laser beams are reflected from the disc surface to the beam splitter 13 through the objective lens 14, and directed to the AF unit 16 after being divided by the beam splitter 13, thereby being utilized for
5 establishing proper focus through movement of the objective lens 14.

The method for establishing and maintaining focus is carried out by known method such as, for example, the knife-edge and astigmatic methods. The unit shown herein above in FIG. 2 is hereinafter referred to as 'initialization head'.

10 The method for initializing recording media disclosed herein is implemented by scanning the initialization head over the recording medium. The detailed conditions of the initialization may be adjusted arbitrarily, and an apparatus therefor is illustrated in FIG. 3 in the case of a disc-shaped recording medium.

15 Referring to FIG. 3, the initialization apparatus according to one embodiment disclosed herein includes at least a spindle mechanism 21 for rotating optical recording medium 19, and an initialization head 20 provided with at least with an actuator for displacing the initialization head.

The laser beam scanning is carried out with the thus constructed
20 apparatus, by rotating the optical recording medium 19 by the spindle mechanism 21 and simultaneously displacing the initialization head 20 in the radial direction of the medium. The laser beams are therefore scanned spirally over the area of the recording medium to achieve initialization.

25 Since the spindle mechanism 21 and initialization head 20 are constructed to be operable in an interlocked manner, the disc rotation and the movement for displacing the initialization head 20 in the radial

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direction are also controlled in this manner.

In addition, these rotating and displacing movements are controlled with the above construction such that the speed, at the location of beam irradiation, of the initialization head 20 relative to the rotating medium portion is maintained to be constant, V . As a result, a constant linear scanning speed is achieved and maintained during medium initialization with laser beam irradiation.

The initialization head 10 may be displaced either from the outer edge to inward of the disc or the other way around during the beam scanning. The initialization is carried out at least over the data recording area on the disc, and may also extend to an area therebeyond.

In order for the recording layer to be adequately initialized throughout the disc area, a displacement step, d , (or the amount of displacement in the direction perpendicular to the disc tracks) of the initialization head 10, and the width at half maximum, W_r , of the spatial laser power distribution in the direction perpendicular to the disc tracks, preferably satisfy the relation, $d < W_r$. That is, the displacement step is smaller than the width at half maximum of the spatial laser power distribution of the laser device at the beam spot.

In addition, the overlap of irradiated portions should be considered. Since such overlapped area portions result in the area irradiated more than once, spatial fluctuation may be created in the initialization effect over the disc area. This spatial fluctuation further results in microscopic reflectivity fluctuation especially at the overlapped portions.

In order to decrease the reflectivity fluctuation, it is preferable for the width of the overlapped portion, $W_r - d$, and the width at half maximum, W_r , of the spatial laser power distribution at the beam spot to satisfy the

relation, $W_r - d < 0.5 W_r$.

The apparatus and process for carrying out the media initialization process disclosed herein are characterized by the energy density to be used therefor, as will be detailed herein below.

5 The output laser power and scanning speed for the media initialization are determined by an energy density input into a recording medium during one scanning period.

The energy density E is expressed by the relation,

$$E = P \cdot V / (S \cdot W_t) = P / (W_r \cdot V),$$

10 where P is output laser power, V scanning speed, S the area on the medium under irradiation, and W_t and W_r the width of the laser beam in the direction along, and perpendicular to, the scanning direction, respectively.

 The energy density value expresses the amount of energy input into the unit area of the recording medium during one scanning period, and this value is therefore directly related to the effect generated on the recording layer by the initialization process.

15 As the energy density E increases, the amount of heat generated in the medium increases, thereby causing an increase in temperature in the recording layer. As a result, the recording layer can be brought into the stable crystalline state.

20 However, using energy density E that is unduly high causes the following difficulties: When amorphous marks are formed on the thus formed crystalline recording layer through further irradiation, edge portions of the marks become more highly crystallized by the heat from the above-mentioned irradiation. As a result, when lands are subsequently overwritten on top of the recorded marks, these marks become so stabilized that they may not be completely erased, thereby causing deterioration in

jitter during the first overwrite step.

The upper limit of the energy density E_{\max} , which assures satisfactory first overwrite characteristics, is selected as, for example, $E_{\max} = 1000 \text{ J/m}^2$. Accordingly, it is necessary for the recording medium disclosed herein be initialized at least under the condition of the energy densities of $E \leq E_{\max}$.

In this context, it is noted E values higher than E_{\max} have been generally adopted previously for media initialization. For example, the E values believed used in practice are in the range of 1100 to 1400 J/m^2 in the case of CD-RW discs having linear recording velocities of 1.2 to 4.8 m/sec. The E values for the initialization as high as the present example are considered to cause the above noted deterioration in jitter during the first overwrite step, especially at high linear velocities.

For unduly low E values, in contrast, the amount of heat input into the recording layer is insufficient to achieve satisfactory crystallization results. Some portions therefore remain non-crystallized and the media reflectivity also remains low.

When the thus formed (or prematurely initialized) medium is subjected to repeated overwrite steps, the crystallization of the premature media portions accelerated with the increase in the number of overwrite cycles, whereby a considerable change in reflectivity results compared with its initial value.

As a result, recorded signal qualities following a large number of overwrite cycles are also considerably changed from initial qualities, thereby resulting in jitter value deterioration after a large number of recording cycles, that is disadvantageous in use for practical recording media.

The lower limit of the energy density, E_{\min} , which alleviates jitter deterioration after a large number of overwrite cycles, is selected as, for example, as $E_{\min} = 600 \text{ J/m}^2$.

5 Accordingly, it is preferable for the recording medium disclosed herein to be initialized at least under the condition of the energy densities of $E_{\min} \leq E$.

The scanning speed, V , has a large effect on unevenness in reflectivity resulting from initialization. For unduly high V values, portions of the recording medium can be left non-crystallized (or
10 prematurely crystallized) more often, which results at least partially from a failure in tracking movements by the focus servo unit, which is, in turn, caused by the high V values. This difference in crystallization has effects on the reflectivity, as indicated earlier, thereby resulting in spatial fluctuation in reflectivity and further causing possible failure in tracking.

15 For unduly low V values, in contrast, the beam irradiation time is prolonged and the recording and dielectric layers in the medium tend to be affected more often by heat damage. As a result, a deterioration in recording characteristics such as jitter, in particular, is caused after a large number of overwrite cycles.

20 Accordingly, it is preferable for the recording medium disclosed herein to be initialized at least under the conditions with respect to the scanning speed V , specified as $V_{\min} \leq V \leq V_{\max}$, with $V_{\min} = 3.5 \text{ m/sec}$ and $V_{\max} = 6.5 \text{ m/sec}$.

25 As to information recording into the thus initialized optical recording medium, the determination of optimum recording power with sufficient accuracy is important for its practical usage as well.

In addition, the use of a high power laser is considered to help improve the efficiency of record/ readout operations for recording media. The present inventors have examined the effect of high power laser beams on the recording medium to thereby find optimum conditions of the laser power through experimentation, which will be detailed herein below.

FIG. 9 illustrates the pulse shape of input light beams of 5T width applied to the phase-change recording medium according to the embodiment disclosed herein, FIG. 10 illustrates the pulse shape of input light beams applied to the phase-change recording medium of Example 1, and FIG. 11 is a block diagram illustrating the major units of the write/readout system disclosed herein.

Referring now to FIG. 11, the write/readout system disclosed herein is configured to carry out write/readout operations of information data onto an optical recording medium 18 in a process including: Rotating the recording medium 18 including a phase-change optical recording disc by a driving mechanism 21 equipped with a spindle motor, activating a light source including a semiconductor laser device by a laser driving circuit 24 used as a light source driving unit, focusing laser beams onto the optical recording medium 18 by an optical system (not shown), irradiating and thereby inducing phase transition in the recording layer, and receiving light beams reflected from the recording medium 18 with an optical pickup 23, whereby the write/readout operations onto the optical recording medium 18 are achieved.

As described above, the write/readout system enables carrying out rewriting as well as the write/readout operations of information data onto an optical recording medium 1 by inducing phase transition in the recording layer through the laser beam irradiation onto the optical

recording medium. In addition, the write/readout system is also provided with a plurality of additional units such as, for example, one for modulating information data signals to be recorded by a modulation unit and another for recording the signals into the recording medium by the write/readout pickup.

The recording unit including the optical pickup writes the information data in terms of the width of recorded 'marks' that is generally referred to as the pulse width modulation (PWM) method. Also, data signals to be recorded are modulated through the modulation unit using clock signals according to either the eight-to-four modulation (EFM) method or modified methods thereof, which are effectively utilized in the data recording for rewritable compact discs, for example.

In data recording into the phase-change recording medium, a "1" signal (i.e., 1 in binary) is carried out, in general, by forming amorphous portions in the recording layer of the recording medium, which is carried out, in turn, by elevating the temperature of the recording layer portion to a level higher than its melting point and subsequently lowering the temperature at a rate high enough to form an amorphous phase.

Referring to FIG. 10, data recording can be achieved using a series of laser pulses delivered to the recording medium. Namely, a pulse fp raises the temperature of a recording layer portion to a level higher than its melting point to thereby form the front portion of the recorded mark, a pulse mp retains the thus raised temperature to thereby form the middle portion of the recorded mark, a the pulse op lowers the temperature of recording layer portion to thereby form the rear portion of the recorded mark.

The amount of beam irradiation onto the recording medium varies with the linear velocity of the rotating recording medium to thereby change the speed of the above-mentioned raising and lowering the temperature of the recording layer portions. Therefore, the speeds of raising and
5 subsequent lowering the temperature of recording layer portions can appropriately be adjusted by varying the linear velocity of the rotating recording medium.

Further, the information pertinent to recorded data by the PWM method is placed at the edge portions of the recorded marks. Therefore,
10 in order to prevent either smearing at the boundary between recorded and non-recorded portions on the recording layer, or undue erasing caused by crystallization of the amorphous recorded portions, it is important to prevent undesirable heating of portions other than those to be recorded.

Smearing prevention, or distinction between portions to be recorded and to be retained at lower (ordinary) temperature, may be achieved by
15 suppressing both undue heat generation at the recording layer portions and controlling heat conduction in the recording layer. By achieving distinction between the recorded and non-recorded portions with the above noted measures, excellent information data signals with reduced jitter
20 values can be obtained.

Having generally described the present disclosure, the following examples are provided further to illustrate preferred embodiments. This is intended to be illustrative but not to be limiting to the materials, apparatuses or methods described herein.

25 Examples 1 through 23 and Comparative Examples 1 through 11 primarily illustrate recording materials and their compositions for forming phase change recording media, while Examples 24 through 26 illustrate

methods and processes for implementing initialization and recording processes on the recording media.

EXAMPLES

5 EXAMPLES 1 through 10, and
COMPARATIVE EXAMPLES 1 through 5

A plurality of phase-change recording media were formed, using sputtering targets, including constituent layers, which will be detailed herein below.

10 The materials composition of sputtering targets used for the layer deposition and the composition of the layers formed by the deposition are given in respective columns in Table 1.

A phase-change recording medium was first fabricated on a polycarbonate (PC) substrate of 1.2 mm thickness, which was provided with guide tracks of a track pitch of 1.6 μm formed with grooves having a depth of approximately 30 nm and a width of approximately 0.6 μm .

The following constituent layers were subsequently formed on the PC substrate in order as follows by sputtering deposition technique using respective sputtering targets: A first dielectric layer of $\text{SiO}_2\cdot\text{ZnS}$ with a thickness of approximately 80 nm, a recording layer of approximately 18 nm thickness, a second dielectric layer of $\text{SiO}_2\cdot\text{ZnS}$ with a thickness of approximately 32 nm, a reflective/ heat dissipating layer of Al alloy containing 1.5 wt % of Ti with a thickness of approximately 160 nm, and a coated layer of UV curing resin with a thickness of approximately 10 μm , whereby a recording medium was formed.

The sputtering deposition of the recording layer was carried out in Ar gas flow of 10 sccm under 3×10^{-3} Torr pressure with RF power of 500

W. In a similar manner, further phase-change recording media were subsequently formed.

The thus formed recording media were then subjected to a data recording process and characteristic measurements. During the
5 measurements, linear velocities for the data recording suitable for respective recording media were selected ranging from 9 m/sec to 30 m/sec.

As to the signal recording, the EFM method was utilized, irradiating with multi-pulsed laser beams during recording. The optical pickup unit presently used had an objective lens of an aperture of NA 0.5 and a
10 semiconductor laser of 780 nm wavelength.

Results obtained from the measurements are shown in Table 1 on the reflectivity and the number of overwrite cycles for respective recording media. The 'x' mark in the overwrite cycle column indicates that an overwrite could not be achieved even though the first recording was
15 feasible.

The results in Table 1 indicate that excellent disc characteristics are obtained for recording layer compositions of a(Ag): b(In): c(Sb): d(Te): e(Ge), with $0.1 \leq a \leq 7$, $2 \leq b \leq 10$, $64 \leq c \leq 92$, $5 \leq d \leq 26$ and $0.3 \leq e \leq 3$, where a, b, c, d and e are the content (atom %) of Ag, In, Sb, Te and Ge,
20 respectively.

The results in Comparative Examples 3 and 5 indicate that the reflectivity value was below 14% for the content, c(Sb)+ d(Te), of less than 88 atom %, whereby the readout compatibility with CD-ROM drive decreased and repeated recording cycle capability deteriorated.

25 In addition, for the content, c(Sb)+ d(Te), of more than 93 atm %, as in Comparative Example 2, reflectivity becomes too high, whereby readout errors increase since signal amplitudes of sufficiently large magnitude

could not be obtained.

Further, on the recording medium with the content as in Comparative Examples 4, 6 and 7, media overwrite could not be achieved at linear recording velocity of 9 m/sec.

- 5 The sputtering targets used for forming the above recording layers of Examples 1 through 10 and Comparative Examples 1 through 5, were prepared respectively first by melting raw constituent materials, then cooling to be solidified materials, crushing or milling, and subsequently sintering.

10

Table 1-1

	Sputtering Target Composition				
	Ag	In	Sb	Te	Ge
Example 1	1.0	9.0	66.0	24.0	0.0
Ex. 2	2.0	7.0	77.0	14.0	0.0
Ex. 3	7.0	4.5	68.5	20.0	0.0
Ex. 4	0.5	5.5	81.5	12.5	0.0
Ex. 5	0.5	2.5	92.0	5.0	0.0
Ex. 6	1.5	9.0	67.5	22.0	0.0
Ex. 7	1.0	6.5	74.5	18.0	0.0
Ex. 8	1.0	7.0	70.0	21.0	1.0
Ex. 9	0.5	7.5	65.0	25.0	2.0
Ex. 10	3.0	5.0	65.0	24.0	3.0
Comparative Example 1	7.0	6.0	63.0	24.0	0.0
Com. Ex. 2	2.0	1.0	93.0	4.0	0.0

Com. Ex. 3	3.0	11.0	66.0	20.0	0.0
Com. Ex. 4	1.0	7.5	63.5	28.0	0.0
Com. Ex. 5	1.0	7.6	63.0	22.5	6.0
Com. Ex. 6	4.5	5.5	62.5	27.5	0.0
Com. Ex. 7	5.5	4.0	63.0	26.5	1.0

Table 1-2

	Layer Composition					Characteristics	
	Ag	In	Sb	Te	Ge	Reflect-ivity (%)	Overwrite cycles
Example 1	0.9	9.1	66.2	23.8	0.0	16	8000
Ex. 2	2.1	6.9	77.1	13.9	0.0	17	5000
Ex. 3	7.1	4.6	68.4	19.9	0.0	15	3000
Ex. 4	0.6	5.5	81.6	12.5	0.0	20	4000
Ex. 5	0.6	2.4	92.1	4.9	0.0	22	5000
Ex. 6	1.5	9.1	67.6	21.8	0.0	15	8000
Ex. 7	1.1	6.6	74.4	17.9	0.0	18	6000
Ex. 8	0.9	7.1	70.0	20.1	0.9	17	4000
Ex. 9	0.6	7.6	64.9	24.9	2.0	16	6000
Ex. 10	3.1	4.9	64.8	24.1	3.1	15	7000
Com. Ex. 1	6.9	6.1	62.9	24.1	0.0	13	300
Com. Ex. 2	2.0	1.1	92.9	4.0	0.0	22	500
Com. Ex. 3	2.9	11.2	66.1	19.8	0.0	12	600
Com. Ex. 4	1.1	7.4	63.4	28.1	0.0	17	×

Com. Ex. 5	1.0	7.6	63.0	22.4	6.0	13	200
Com. Ex. 6	4.4	5.6	62.4	27.6	0.0	16	×
Com. Ex. 7	5.4	4.1	62.9	26.6	1.0	15	×

EXAMPLE 11

Several phase-change recording media were formed each including recording layers which were deposited using the sputtering target of Example 1. In addition, the sputtering deposition of respective recording layers was carried out in Ar gas atmosphere mixed with 0, 6, 10 or 15 mol % of gaseous nitrogen.

The composition of the thus formed recording layers was subsequently obtained. In addition, the recording layers were each incorporated into recording media and the overwrite characteristics of these media were also measured. The results from these measurements on the recording layer composition and overwrite cycle number are shown in Table 2.

Table 2

N ₂ /(Ar+N ₂) (mol %)	Content (atom %)					Overwrite cycles
	Ag	In	Sb	Te	N	
0	2.1	6.9	77.1	23.9	0	5000
6.0	1.7	6.6	76.3	23.4	2.0	4000
10.0	1.5	6.4	75.2	22.9	4.0	800
15.0	1.4	6.3	74.7	22.6	5.0	200

The results included in Table 2 show that the number of feasible overwrite cycles sharply decreases for nitrogen contents in excess of 10 mol %.

5 EXAMPLES 12 through 23, and
 COMPARATIVE EXAMPLES 8 through 11

 Several phase-change recording media were formed using the sputtering target of Example 1 in a similar manner to Examples 1 through 10 and Comparative Examples 1 through 5.

10 The recording media each included layers deposited on a polycarbonate substrate of 1.2 millimeter thickness, such as a first dielectric layer of $\text{SiO}_2\text{-ZnS}$ with a thickness of approximately 90 nm, a recording layer of approximately 18 nm thickness, a second dielectric layer of $\text{SiO}_2\text{-ZnS}$ with a thickness of approximately 34 nm, and a reflective/
15 heat dissipating layer of approximately 160 nm thickness. The reflective/heat dissipating layers for forming respective recording media were each formed herein with metal or alloy layers having the composition shown in respective columns in Table 3.

 When the thus formed recording media were subsequently subjected
20 to measurements of reflectivity, overwrite cycle number and storage durability, the results were obtained as shown in Table 3. For storage durability, the measurements were made at 80 °C and relative humidity of 85%. The mark 'x' in Table 3 indicates that an increase in errors was
25 found after 300 hours in storage.

Table 3

	Reflective layer (atom %)	Reflect- ivity (%)	Overwrite cycles	Storage durability
Ex. 12	Al99.5Ti0.5	19	2000	o
Ex. 13	Al97.5Ti2.5	17	3000	o
Ex. 14	Al98.5Ta1.5	18	3000	o
Ex. 15	Al98.5Cr1.5	17	2500	o
Ex. 16	Al98.5Si1.5	19	1500	o
Ex. 17	Al98.5Ti1.0Ta0.5	18	3000	o
Ex. 18	Ag100	20	3000	o
Ex. 19	Ag98Pd2	18	4000	o
Ex. 20	Ag98Cu2	19	3000	o
Ex. 21	Ag98Au2	19	5000	o
Ex. 22	Ag98Pt2	19	4000	o
Ex. 23	Ag96Pd2Cu2	17	3000	o
Ex. 24	Ag98Ru2	18	4000	o
Ex. 25	Ag98Ti2	19	5000	o
Com. Ex. 8	Al95Ti5	14	200	o
Com. Ex. 9	Al99Mg1	18	100	×
Com. Ex. 10	Al98.5Cu1.5	14	300	×
Com. Ex. 11	Ag94Pd6	13	200	o

The results included in Table 3 show that (1) reflective/ heat dissipating layers each essentially consisting of Al yield satisfactory media characteristics, when at least one kind of element selected from the group consisting of Ta, Ti, Cr and Si is included therein with its content ranging
5 between 0.3 to 2.5 wt %, and (2) the metal or alloy layers used as reflective/ heat dissipating layers each essentially consisting of Ag exhibit excellent overwrite characteristics and storage durability, when at least one kind of element selected from the group consisting of Au, Pt, Pd, Ru, Ti and Cu is included therein with its content ranging between 0 to 4 weight
10 percent.

EXAMPLE 24 II

In order to examine initialization process steps and conditions therefor, a CD-RW recording medium was formed.

15 As illustrated in FIG. 1, this recording medium includes at least a polycarbonate substrate provided with guide tracks of a continuous spiral groove for use in CD-RW discs, and constituent layers formed thereon in order as follows: A first dielectric layer, a recording layer, a second dielectric layer, a reflective layer, and a protective layer.

20 The first and second dielectric layers were deposited by PF sputtering using sputtering targets of $\text{SiO}_2 \cdot \text{ZnS}$ composition, and the recording layer was formed by DC sputtering using a sputtering target of AgInSbTe alloy composition. In addition, the reflective layer was formed by DC sputtering using a sputtering target of Al and Ti, as major
25 components.

The first dielectric layer had a thickness of 80 nm, the recording layer was 20 nm thick, the second dielectric layer was 30 nm thick, and the

reflective layer and protective layer were 150 nm thick.

Spin coating a layer of UV curing resinous material on the recording medium, and hardening by UV irradiation, completed the formation of the recording medium.

5 This recording medium was subsequently subjected to initialization process steps using an initialization apparatus equipped with an initialization head operated under the following conditions:

$\lambda = 810$ nm in laser wavelength for initialization,

10 $R_r = 100$ μ m for the length of laser beam along the radial direction (or W_r along the major axis),

$R_t = 1.0$ μ m along the tangential direction, and

$d = 60$ μ m for distance of head displacement.

15 The conditions of medium initialization were shown in Table 4. It was found that auto-focusing was not feasible with an initialization power of less than 330 mW, whereby media initialization was unfeasible.

20 It was found that the CD-RW recording media formed as above have satisfactory media characteristics as high speed CD-RW discs capable of carrying out read/write/erase operations according to Orange Book specification (Part III, Vol. 2) at linear recording velocities ranging CD4 \times to CD10 \times speed.

25 Subsequently, data recording steps were carried out onto the initialized recording media according to the Orange Book specification, in which Spin Tester DDU1000 from PulseTech Co. was used as a CD-RW measurement apparatus equipped with an optical pickup unit under the following conditions:

$\lambda = 795$ nm in laser wavelength for recording,

NA = 0.5,

Linear recording velocity = 12.0 m/sec (CD10×), and

Coding : EFM.

For the recording, the beam power used ranged from 19 mW to 21 mW, again according to the Orange Book specification, and the results on first direct overwrite (DOW 1) and direct overwrite after 1000 cycles (DOW1000) were primarily obtained. The recorded signals were then readout with the Spin Tester DDU1000 and, 3T land jitter was measured. The results obtained on the readout signals are shown in Table 4.

Table 4

Initialization conditions			Characteristics of recorded signals			
V (m/sec)	P (mW)	E (J/m ²)	Initial 3T LJ	DOW 1 3T LJ	DOW 1000 3T LJ	ΔRgh
3	330	1100	20.2	37.4	35.8	0.04
3	385	1283	19.9	42.8	38.5	0.04
3	440	1467	20.1	49.5	42.2	0.03
3	495	1650	21.2	54.9	44.5	0.04
3	550	1833	21.5	61.8	46.5	0.04
4	330	825	21.3	25.3	26.0	0.06
4	385	963	20.9	28.2	27.3	0.06
4	440	1100	20.0	35.8	30.0	0.05
4	495	1238	18.8	46.5	32.2	0.05
4	550	1375	18.5	55.3	34.4	0.04
5	330	660	22.2	24.9	27.7	0.08

5	385	770	21.5	23.8	28.3	0.07
5	440	880	22.2	25.5	26.6	0.05
5	495	990	23.1	28.1	27.2	0.05
5	550	1100	22.2	36.7	28.9	0.04
6	330	550	27.2	27.8	24.3	0.12
6	385	642	24.1	26.2	25.5	0.10
6	440	733	24.0	24.7	27.3	0.08
6	495	825	23.1	23.9	27.5	0.07
6	550	917	23.2	25.1	28.8	0.07
7	330	471	30.2	32.2	27.2	0.45
7	385	550	27.1	28.1	27.5	0.43
7	440	629	25.2	25.9	28.2	0.32
7	495	707	22.1	24.8	27.8	0.30
7	550	786	22.2	23.6	28.3	0.22

DOW: Direct OverWrite, LJ: Land Jitter

The 3T land jitter was measured with varying initialization power P and scanning speed of the initialization head V , and the results from the measurements are shown also in FIG. 4. The results indicate that jitter increases with decrease in P and V . The magnitude of energy density E is plotted as a function of P and V in FIG. 5.

When the values shown in FIGS. 4 and 5 are compared, it is found that DOW 1 jitter tends to increase with decreasing energy density E . The range found for the E value is $E > 1000 \text{ J/m}^2$, for which jitter exceeds

the 35 nsec that is specified as a standardized jitter value in the Orange Book.

Similarly, 3T land jitter after 1000 cycles of direct overwrite (DOW1000) was measured with varying initialization power P and scanning speed of the initialization head V , and the results from the measurements are shown also in FIG. 6.

When the values shown in FIGS. 6 are compared with those in FIG. 5, it is found the DOW 1000 3T land jitter tends to increase with decreasing energy density E . Also found is the range of the E value, $E < 600 \text{ J/m}^2$, for which jitter exceeds the 35 nsec that is specified in the Orange Book.

The results indicate that satisfactory values for both DOW1 and DOW1000 3T land jitter are obtained for E values in the range of $600 \text{ J/m}^2 \leq E \leq 1000 \text{ J/m}^2$, whereby CD-RW discs can be prepared with excellent overwrite characteristics.

Furthermore, as shown also in Table 4, DOW1000 3T land jitter remains relatively high for scanning speed of 3 m/sec regardless P values, and the overwrite characteristics are found to be improved by satisfying the relation, $V \geq 3.5 \text{ m/sec}$.

The change in disc reflectivity, ΔR_{gh} , was obtained at the time immediately after the initialization and prior to recording as follows. Namely, reflectivity values of the disc reflectivity, R_{gh} , were measured over the disc area prior to recording, to thereby yield several reflectivity values such as R_{max} , R_{min} and R_{avg} for its maximum, minimum, and average, respectively.

The change in disc reflectivity, ΔR_{gh} , is then calculated by the equation, $\Delta R_{gh} = (R_{max} - R_{min}) / R_{avg}$. Therefore, as the fluctuation in disc reflectivity over the disc area increases, the change in disc reflectivity

or reflectivity fluctuation, ΔR_{gh} , increases. The ΔR_{gh} values were measured with varying initialization power P and scanning speed of the initialization head V , and the results from the measurements are shown in FIG. 7.

5 Since a reflectivity fluctuation ΔR_{gh} exceeding 0.1 increases tracking error signals, failure in precise tracking such as off-tracking may be caused. This difficulty is alleviated by satisfying the relation with the scanning speed V , $V \geq 3.5$ m/sec, thereby decreasing the fluctuation. As a result, the range of suitable P, V values corresponding to the above noted
10 results is shown with as the shaded area in FIG. 8.

EXAMPLE 25

In order to obtain an optimum recording power, recording process steps were carried out onto a phase-change optical recording medium.

15 The recording medium was prepared including at least the following layers which were formed in order as follows: A first dielectric layer of $\text{SiO}_2 \cdot \text{ZnS}$ with a thickness of approximately 90 nm, an AgInSbTe recording layer of approximately 18 nm thickness, a second dielectric layer of $\text{SiO}_2 \cdot \text{ZnS}$ with a thickness of approximately 32 nm, and an Al alloy layer
20 of approximately 160 nm thickness.

The thus formed recording medium was subsequently subjected to data recording with linear recording velocity of 12.0 m/sec by means of an optical pickup unit having an aperture of NA 0.5 and laser emission of 790 nm in wavelength. In addition, the signals generated after the EFM
25 method were input for data recording.

The results in FIG. 10 show that satisfactory values were found as $S = 1.25$, $R = 1.20$, thereby leading to $P_s = 18 \text{ mW}$. As a result, the optimum was obtained as $P_o = 21.6 \text{ mW}$.

5 EXAMPLE 26

In order to select optimum recording power, recording process steps were carried out onto a phase-change optical recording medium.

The recording medium was prepared in a similar manner to that of Example 25. In addition, information on S and R values, corresponding
10 to the above noted relations $S = 1.25$ and $R = 1.20$, are recorded in advance in the recording medium.

The thus recorded information is subsequently readout to be utilized as the parameters for selecting an optimum recording power. Using the above noted parameters, the optimum was then found as $P_o = 21.8 \text{ mW}$. In
15 addition, repeated recording cycle steps were carried out with this recording power, whereby recording was achieved with sufficient stability without deteriorating the readout signal quality.

The process steps set forth in the present description on the constituent layer deposition and various recording media measurements
20 may be implemented using conventional general purpose microprocessors, programmed according to the teachings in the present specification, as will be appreciated by those skilled in the relevant arts. Appropriate software coding can readily be prepared by skilled programmers based on the teachings of the present disclosure, as will also be apparent to those skilled
25 in the relevant arts.

The present disclosure thus includes a computer-based product which may be hosted on a storage medium, and includes instructions which

can be used to program a microprocessor to perform a process in accordance with the present disclosure. This storage medium can include, but is not limited to, any type of disc including floppy discs, optical discs, CD-ROMs, magneto-optical discs, ROMs, RAMs, EPROMs, EEPROMs, 5 flash memory, magnetic or optical cards, or any type of media suitable for storing electronic instructions.

It is apparent from the above description including the examples that the AgInSbTe phase-change recording medium disclosed herein has material compositions suitable for attaining sufficient sensitivity during 10 writing or erasing operation, preventing a decrease in the erasure ratio and improving the durability of the media properties at high and multiple linear recording velocities with excellent overwrite characteristics.

By the methods disclosed herein for initializing the recording medium, the initialization steps can be carried out with appropriate beam 15 intensities, to thereby decrease unevenness in reflectivity resulted from the initialization, as well as in the initialization effect in the layer caused by overlap of repeated exposures to the beam irradiation.

The thus initialized recording media are found to have desirable disc properties such as low overwrite jitter and decreased fluctuation in disc 20 reflectivity over the disc area, thus assuring high and multiple speed recording capabilities of the recording media.

Furthermore, in the method disclosed herein for determining optimal recording powers, the power can suitably be determined considering the effect of both amplitude m of recorded signals and recording power W , 25 especially in relatively high range of the recording power. This helps obviate previous difficulties of minute adjustments of recording power for each apparatus in the production line.

Numerous additional modifications and variations of the
embodiments described above are possible in light of the above teachings.
It is therefore to be understood that within the scope of the appended
claims, the present invention may be practiced other than as specifically
5 described herein.

This document claims priority and contains subject matter related to
Japanese Patent Applications No. 2001-2258, 2001-5734 and 2001-57392,
filed with the Japanese Patent Office on January 10, 2001, January 12,
2001 and March 1, 2001, respectively, the entire contents of which are
10 hereby incorporated by reference.

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